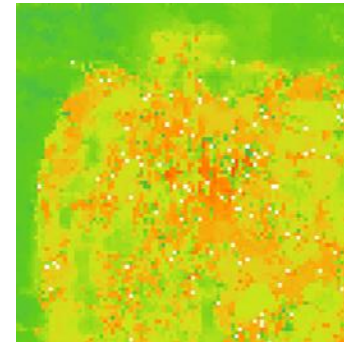
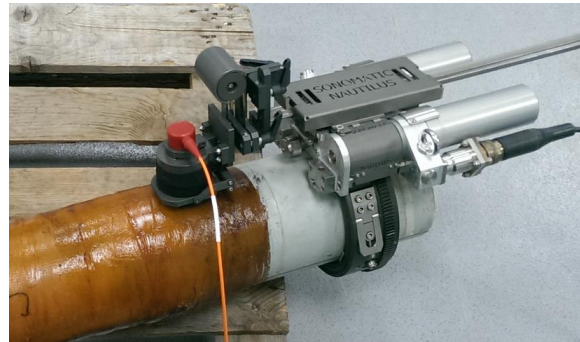
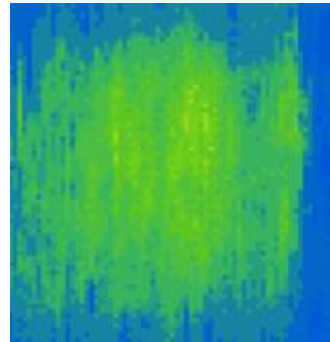
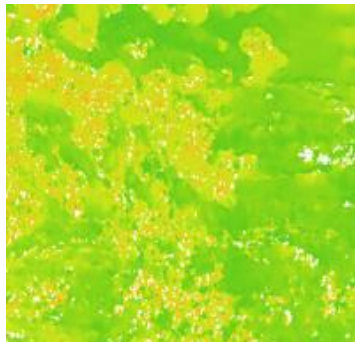


DRS Inspection For Challenging Coatings

Dr Alison Craigon

May 2018



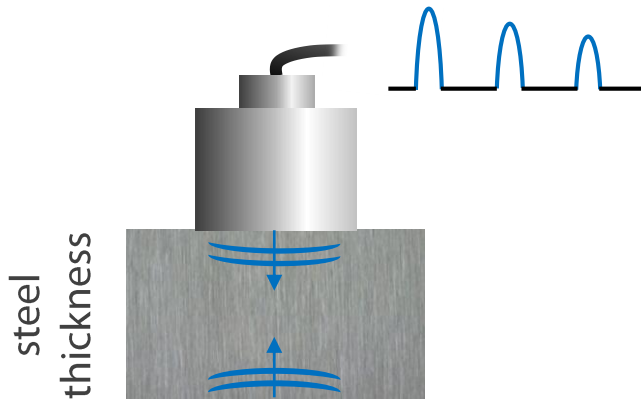
Conventional UT

Accurate measurements of steel thickness are based on reflections using

- High frequency (5 – 10 MHz) signals
- Speed, distance, time calculations

However, many coatings attenuate high frequency signals

→ *Conventional UT often not possible*

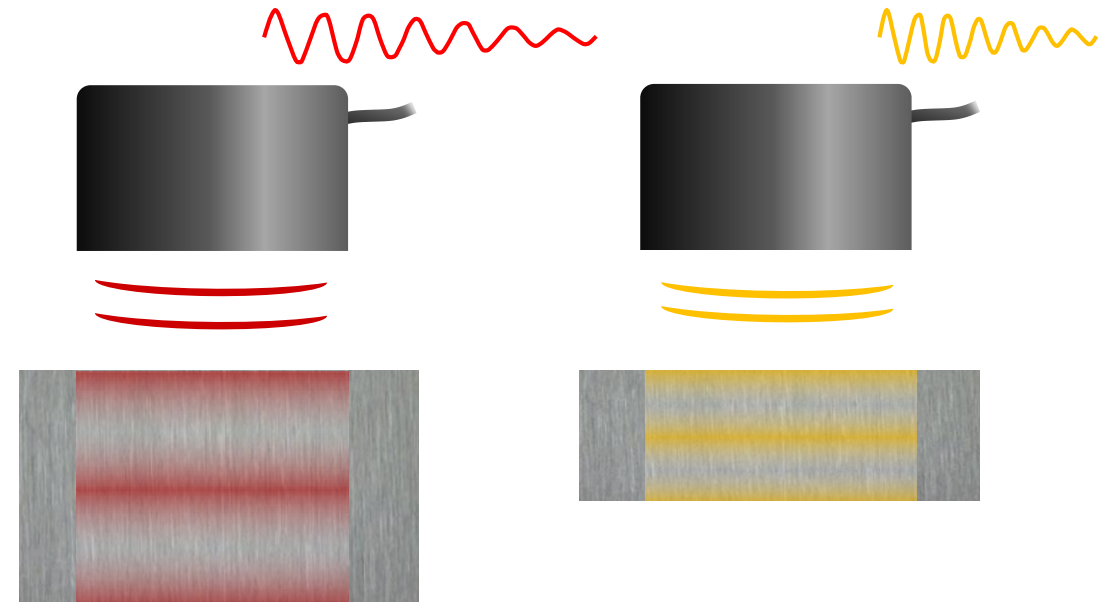


Time-based WT measurements

The DRS Technique

Uses lower frequency ultrasound to make accurate measurements of steel WT

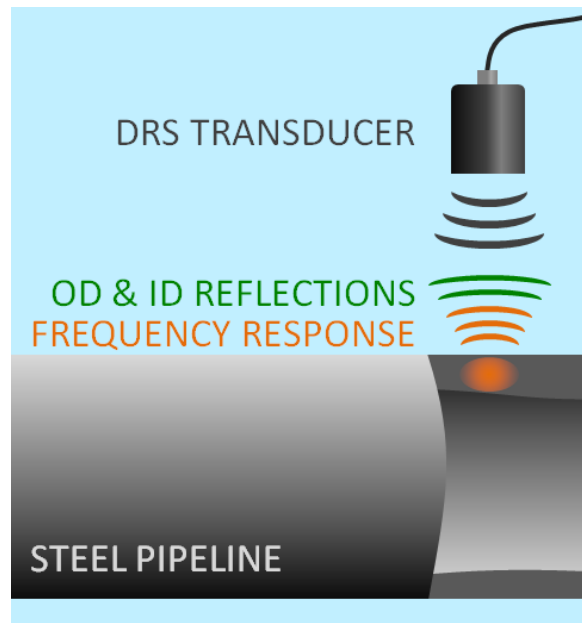
- Low frequencies penetrate coatings more easily
- Low frequencies cause steel to vibrate at its natural frequencies (usually < 1 MHz)
- Vibration frequencies are used to calculate steel WT



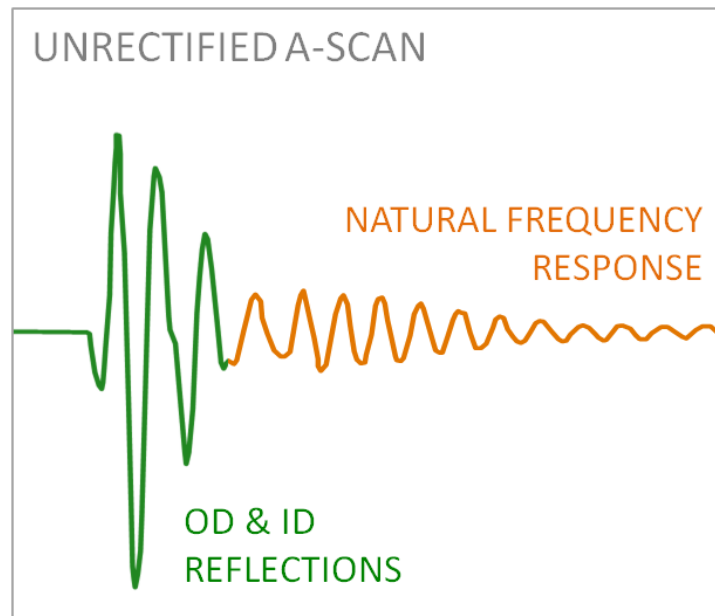
Frequency-based WT measurements

The DRS Technique

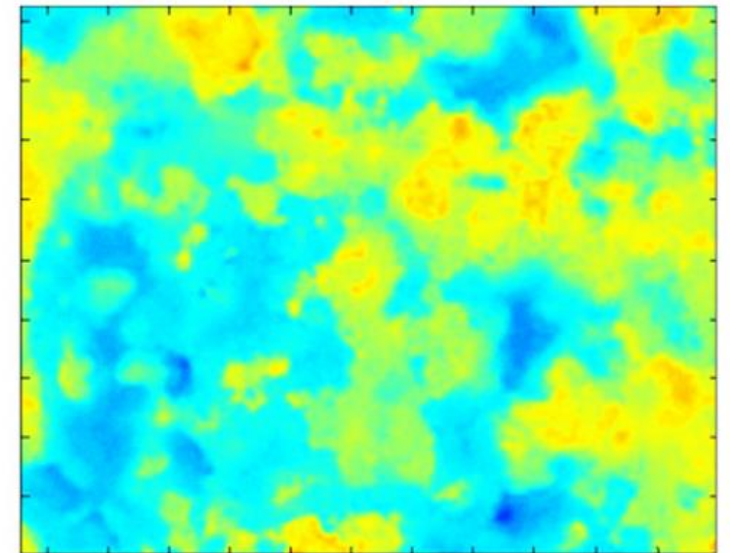
Probe excites steel with a broad range of low ultrasonic frequencies



Steel responds, vibrating at natural frequencies related to the WT



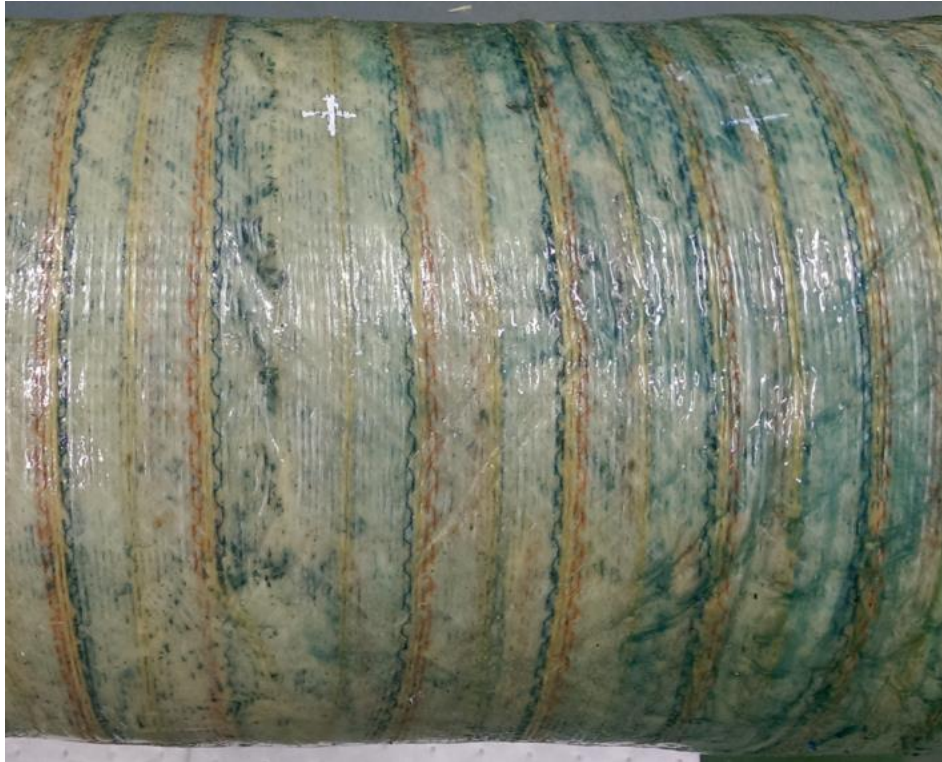
Probe rasters over area collecting response signals



Advanced signal processing algorithms extract the vibration frequencies and map the WT profile

DRS Inspection Through Composite Repairs – Ex-Service Sample

Technowrap 2K™ composite repair

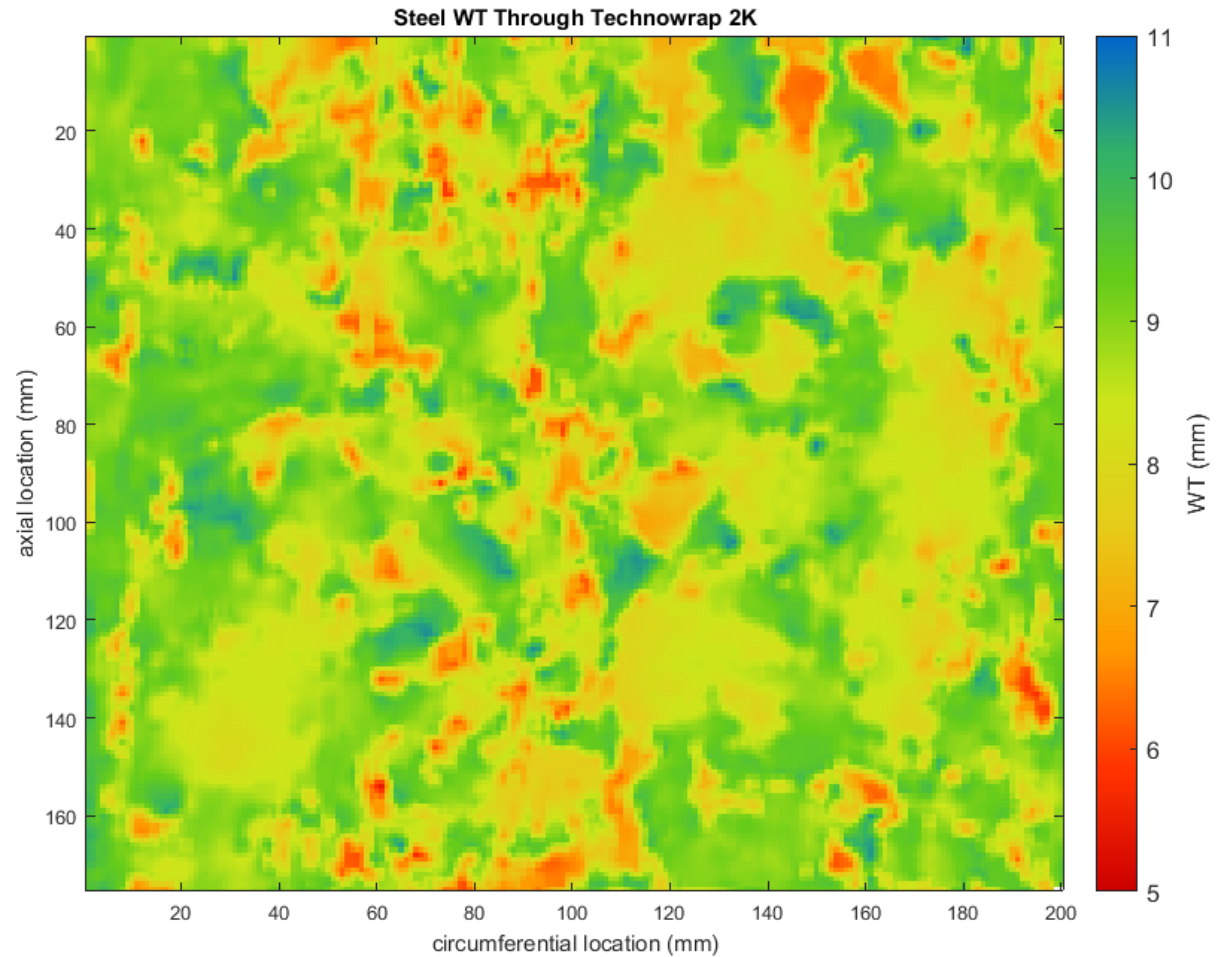


Uneven surface

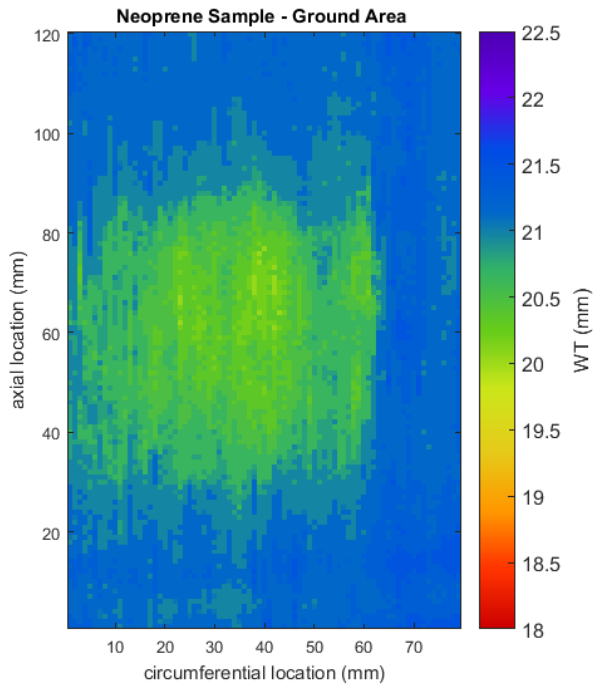
Severe internal corrosion



DRS Inspection Through Composite Repairs – Ex-Service Sample



The DRS Technique – Advantages & Limitations



Steel WT measurement accuracy is typically ± 0.5 mm (80% tolerance)

WT variations of < 1 mm can be measured

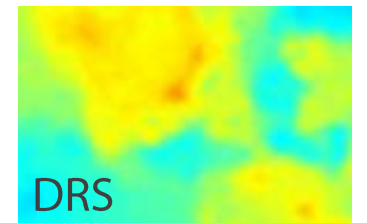
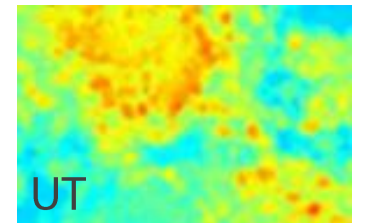
Pits smaller than 10 mm in diameter are not detected

- Weak response from very small features masked by stronger response from neighbouring features

Max steel WT = 22 mm (currently)

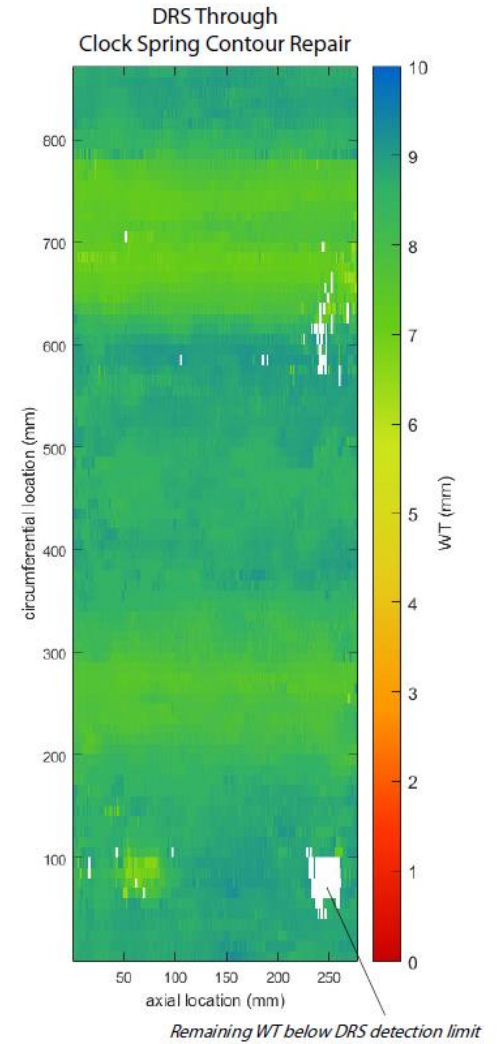
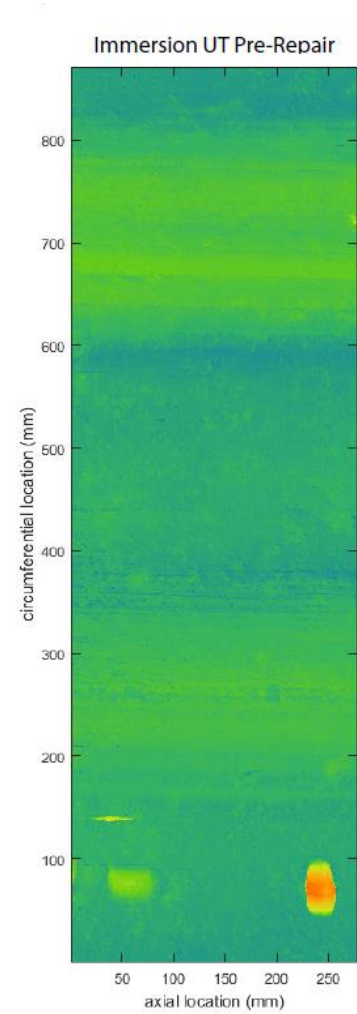
Min measurable steel WT = 3 mm (coating dependent)

- Thin steel has high frequency response which is attenuated in coatings
- Steel WTs reported as 'below detection limit'

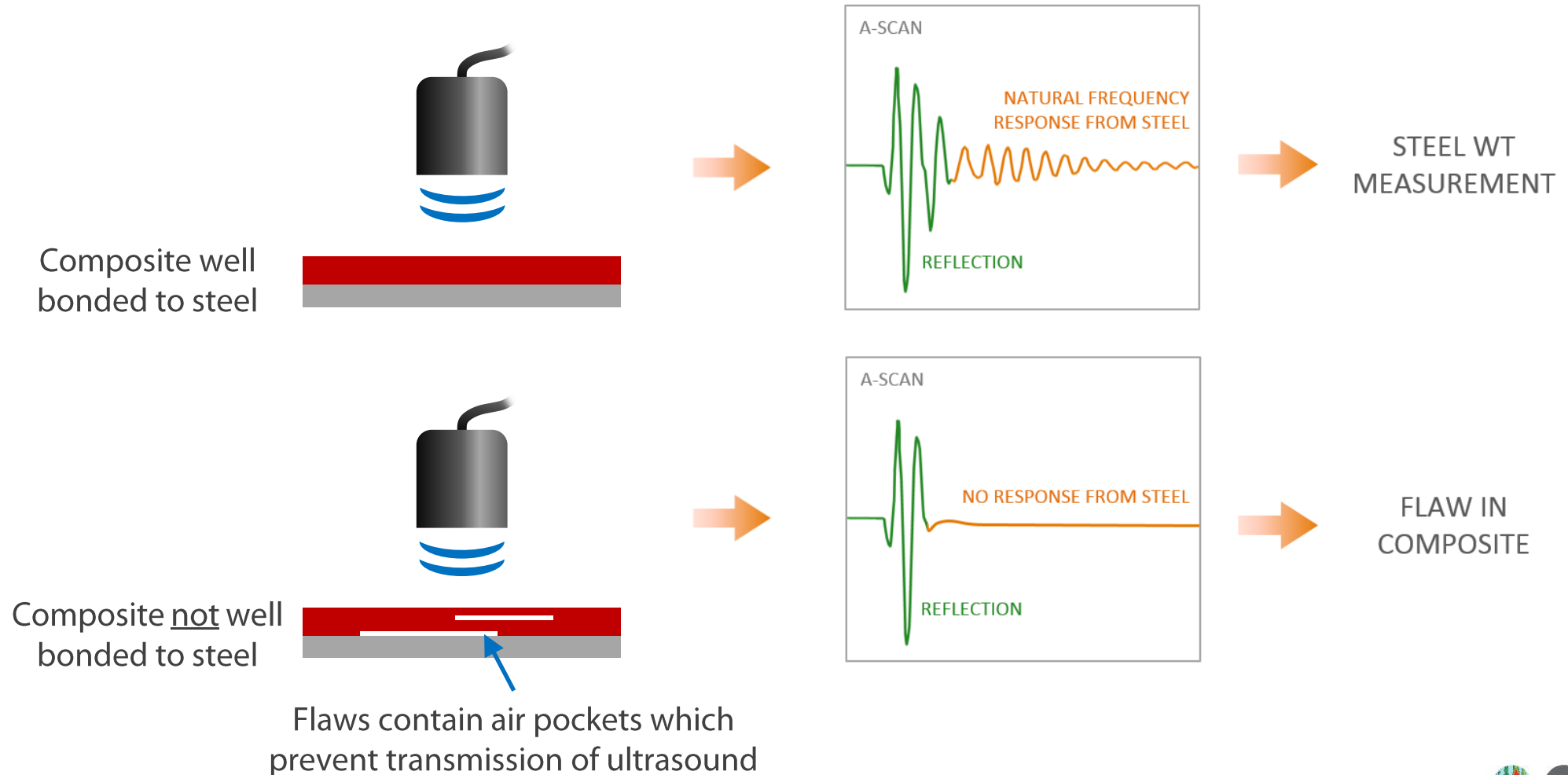


DRS Inspection Through Composite Repairs – Clock Spring[®] Contour

Immersion UT Pre-Repair



Composite Repair Flaw Detection With DRS



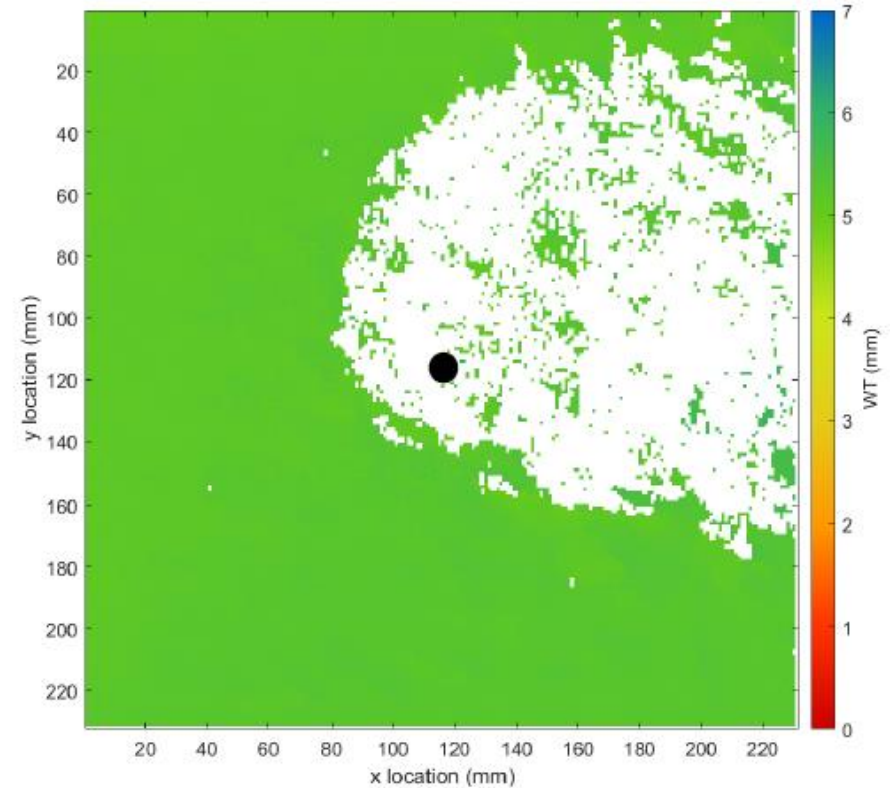
Composite Repair Flaw Detection With DRS – HOIS Trial



Composite repair on a flat plate

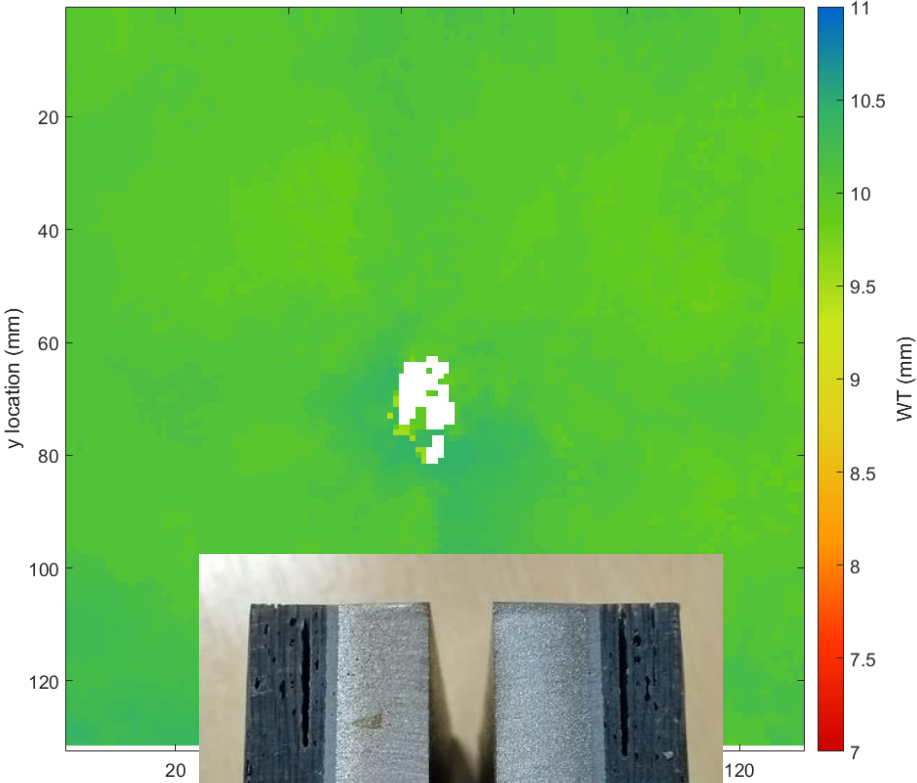
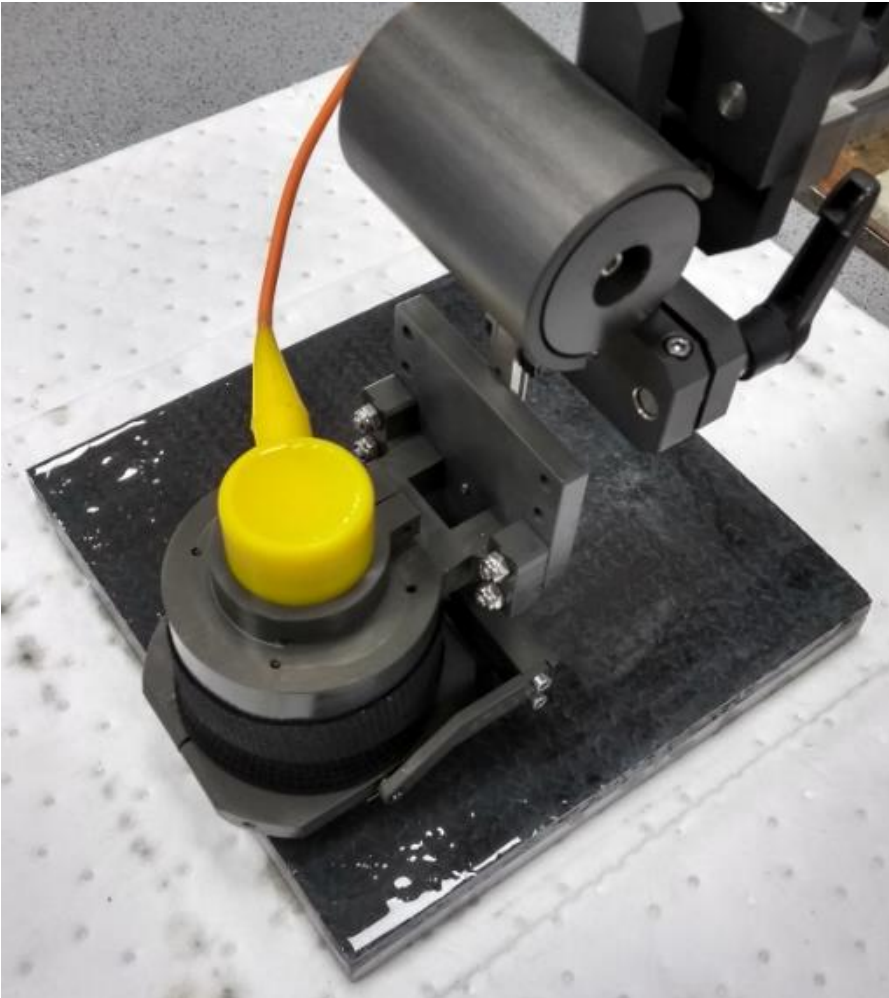


Pressure applied through back of plate to delaminate the composite

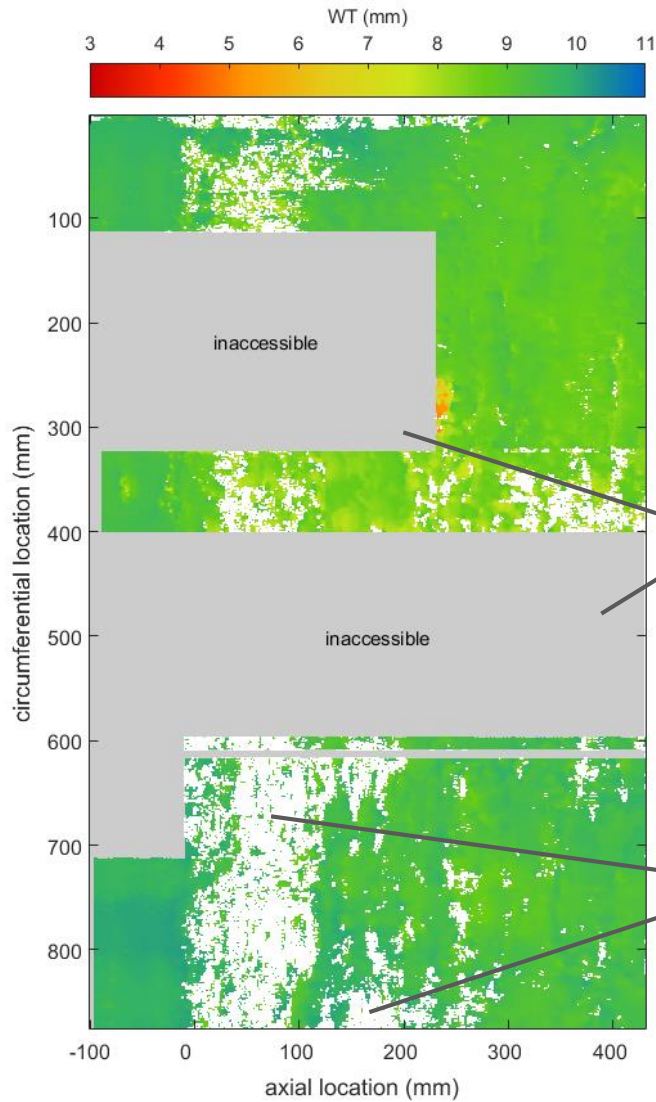


DRS map shows delamination in white

Composite Repair Flaw Detection With DRS – Belzona SuperWrap II

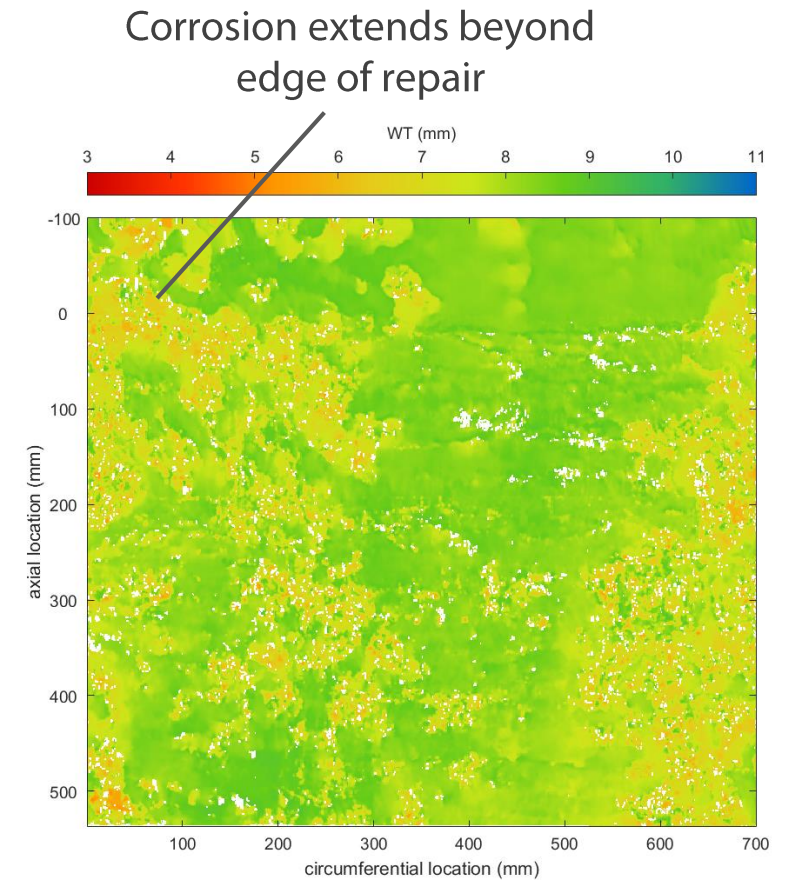


Technowrap 2K™ Composite Repair – DRS Field Trial

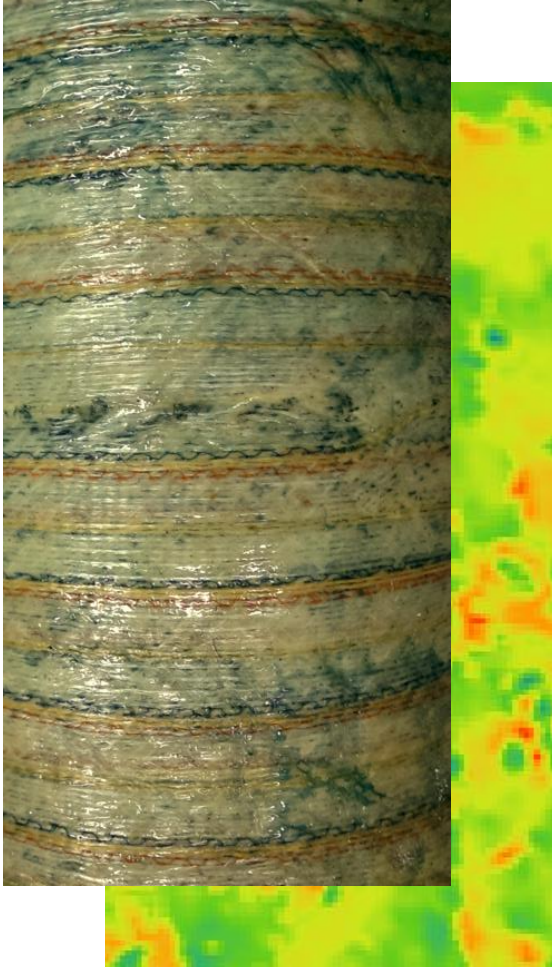


New low-profile scanner can access these areas

Flaws in composite repair



Benefits of DRS Inspection



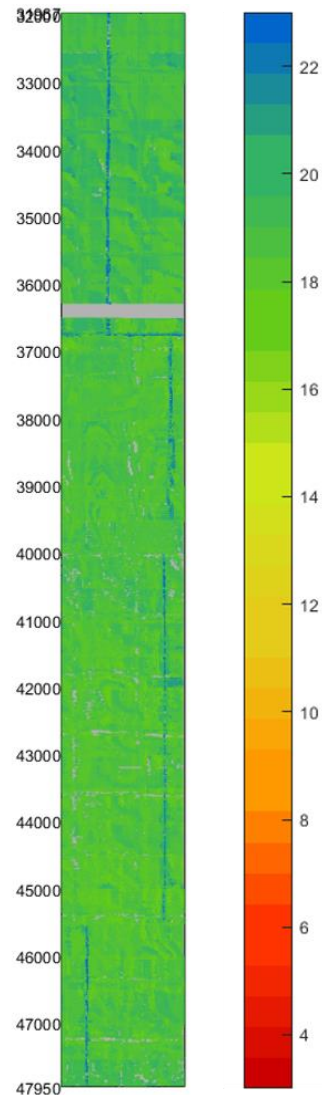
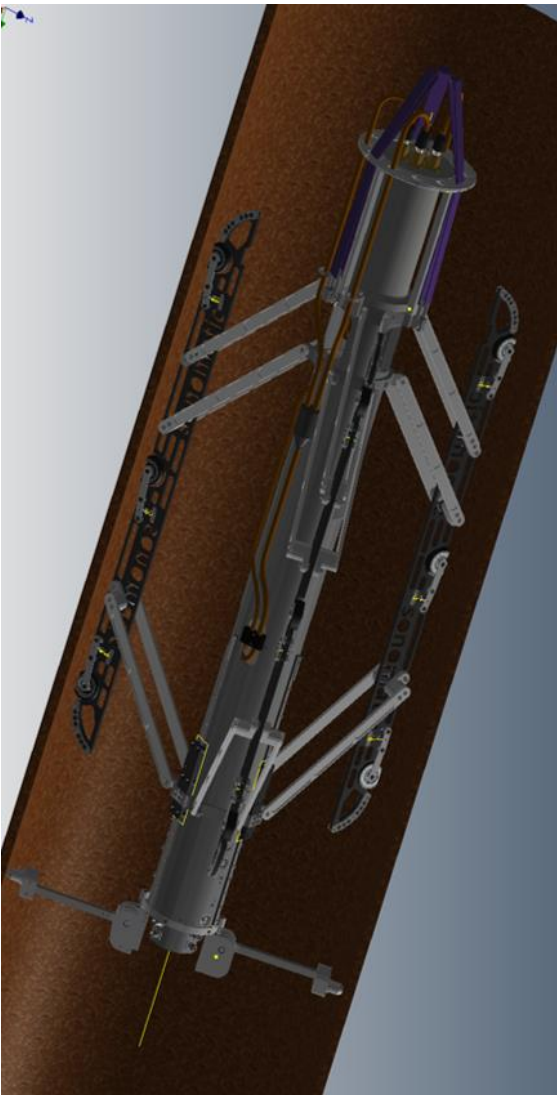
Identifies flaws in composite repairs

The high accuracy of DRS maps makes them suitable for

- Confirming absence of steel degradation
- Quantifying extent of steel wall loss
- Determining if corrosion growth is active
- Estimating corrosion growth rates
- Input to Fitness for Service assessment, including Level 3 using finite element analysis

Neoprene Lined Caisson – DRS Job – UK

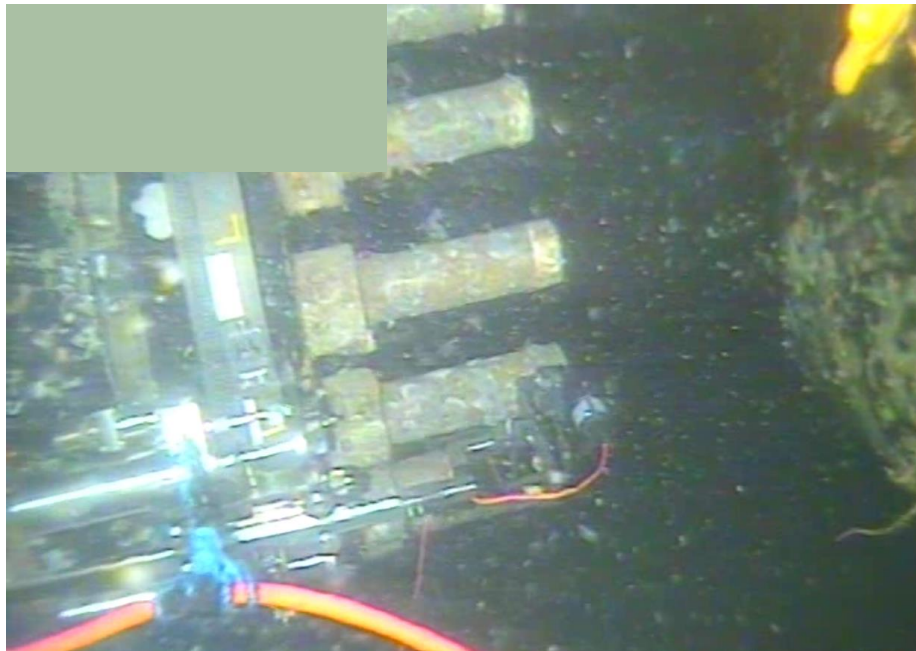
DRS deployed on
Internal Caisson Tool
(ICT)



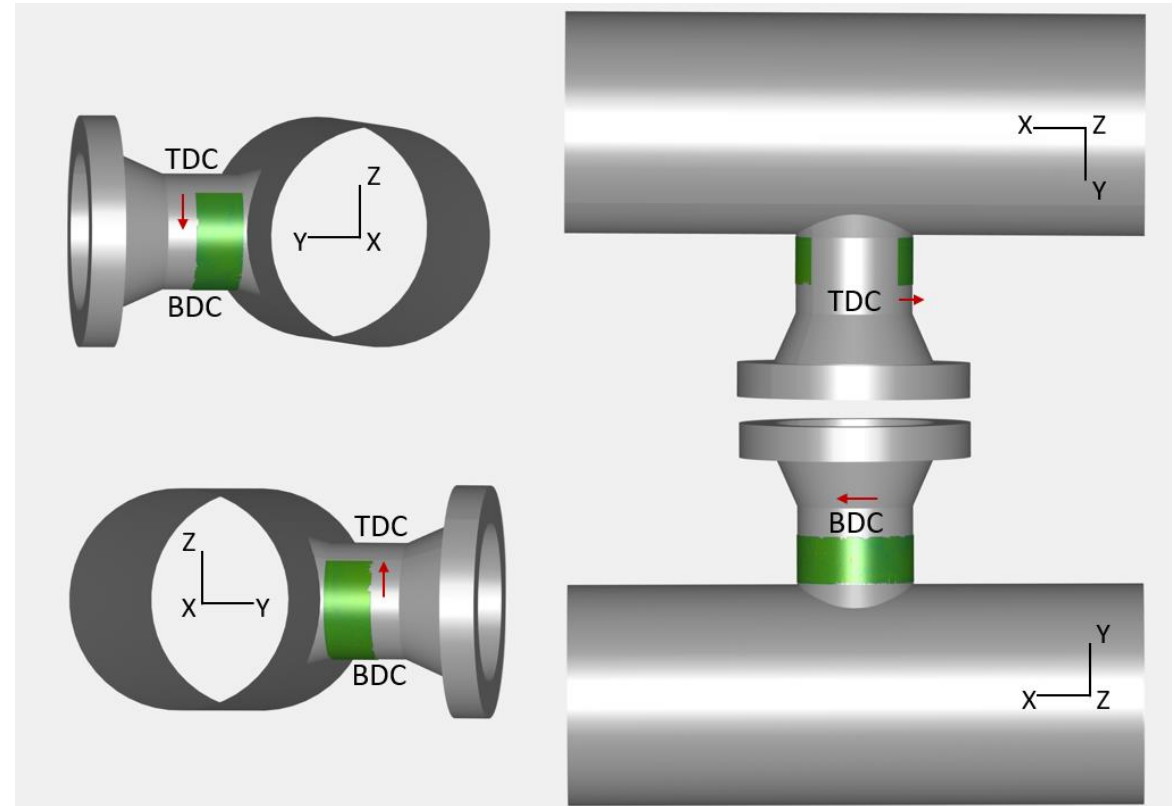
Found no wall loss
• welds are evident
in blue

Coal Tar Enamel Coated Dead Leg – DRS Job – UK

Restricted access to dead leg
between bolts and main line

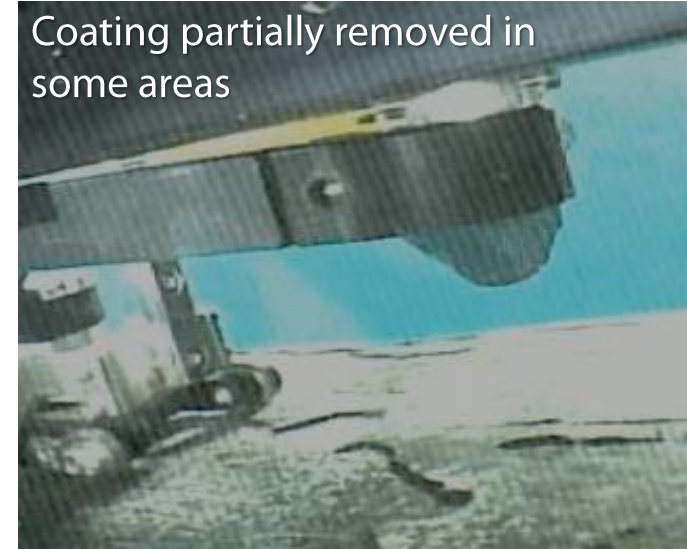
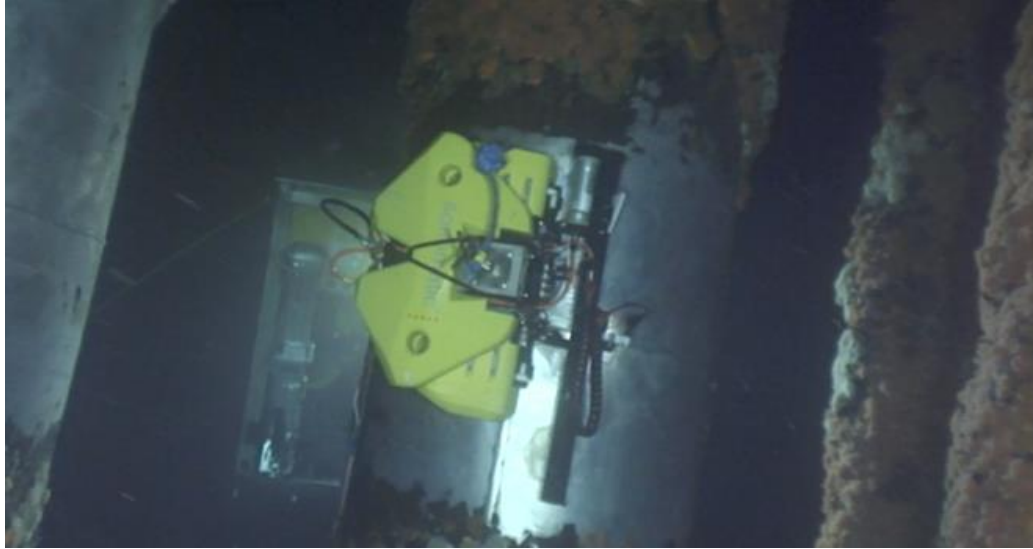


Corrosion mapping with
automated Nautilus scanner

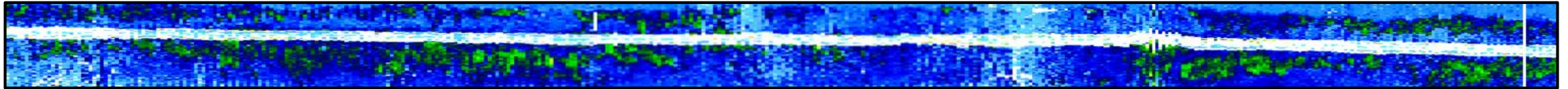


DRS showed no evidence of active wall loss
(nominal WT in green)

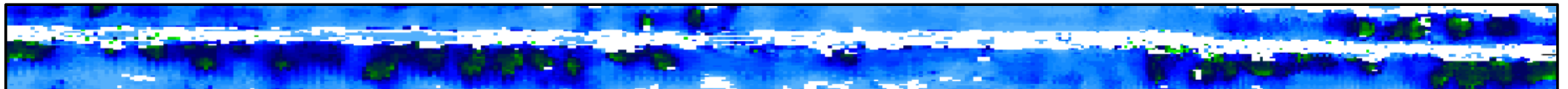
Coal Tar Enamel Coated Caisson – DRS & UT Job – UK



UT



DRS



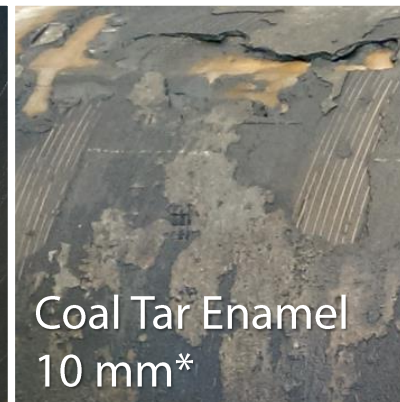
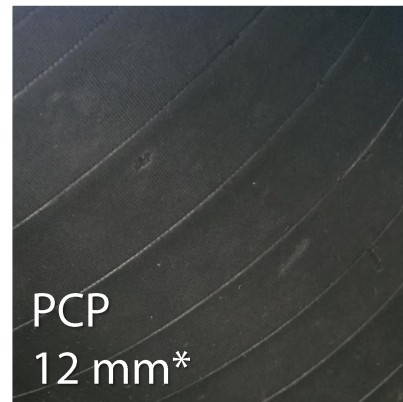
DRS signals are less affected by poor surface condition, results show some wall loss near weld.

DRS Applications

Topside /
Onshore



Subsea



*Thickest samples inspected so far, thicker coatings may be possible.

Several other coating types are currently under evaluation